Complex Renewable Energy Networks Summer Semester 2017, Lecture 13

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Admin

I've been assured that the course will be allowed 4 CPs for the lectures and tutorial.

If you are interested in writing your BA or MA thesis on the topic of Complex Renewable Energy Networks, just write to me or Prof. Stefan Schramm(schramm@fias.uni-frankfurt.de). The oral exam will take place on 25/26/27 July 2017 at FIAS, Uni Campus Riedberg.

Grid Dynamics and Synchronization

So far we have considered the power system only in its static steady state (or hourly snapshots of the steady state), i.e. where the time derivatives of all system quantities are zero.

However, the power system is changing all the time, both in slow, predictable ways (the load changing in a statistically-smoothed way) and in sudden, unpredictable ways, e.g. if a generator fails and 500 MW is lost, or if a power line or transformer fails while heavily loaded (e.g. due to lightning, trees falling, diggers or human operator error). The continental European is designed to survive the sudden loss of 3 GW of generation.

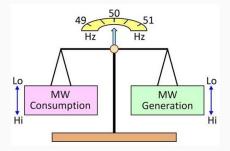
In the next few slides we will look at the dynamics of the power system.

Dynamic phenomena in power systems can be classified by the time scales on which they occur, for example:

- 1. Electro-magnetic transients (e.g. switching, lightning strikes) (100 $\,$ Hz MHz)
- 2. Electro-mechanical swings (e.g. rotor swings in synchronous machines) (0.1 3 Hz)
- 3. Non-electric dynamics (e.g. mechanical phenomena and thermodynamics) (up to tens of Hz)

We will focus on number 2, i.e. frequency dynamics due to interactions between changing loads and rotating machines (generators and motors).

Balancing Power via Steady Frequency

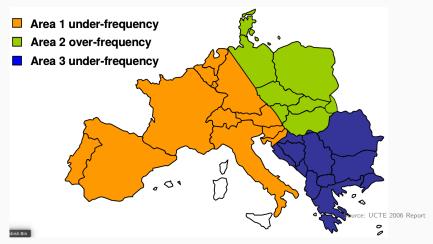


Generation and demand have to be kept in balance at all times (since we cannot create or destroy energy). This is reflected in the alternating current grid frequency (50 Hz in Europe and most of Africa/Asia; 60 Hz in much of Americas). If there is more generation than load, the extra energy is converted to rotational energy of the synchronous rotating machines and the frequency goes up. If there is more load than generation, the deficit energy is substituted by rotational

energy of the synchronous rotating machines and the frequency goes down.

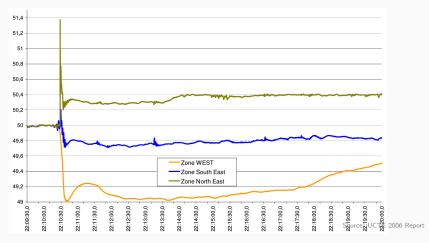
Example: Grid split and partial blackout 4.11.2006

On 4th November 2006 a cascading line outage caused the continental European network to split into three parts. The individual parts were not perfectly balanced: excess generation in North-East, too little in West.

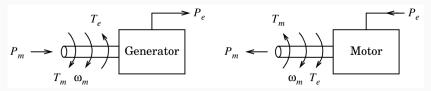


Example: Grid split and partial blackout 4.11.2006

The frequency was only stabilised by load shedding (blackouts) once the frequency hit 49 Hz in the West.



For a single synchronous machine (left in generation mode; right in motor mode) we will now examine the relation between the mechanical power P_m , the electrical power P_e , the frequency ω , the angle θ and the mechanical and electrical torques T_m , T_e .



For the rotor dynamics we have for the moment of inertia J

$$J\frac{d^2\theta}{dt^2} = T_m - T_e$$

Source: Göran Andersson lecture notes

Multiplying by the frequency $\omega = \dot{\theta}$ we get the swing equation

$$\omega J \frac{d^2 \theta}{dt^2} = P_m - P_e$$

The total inertia is given by $H = \frac{1}{2}\omega^2 J$ so we get

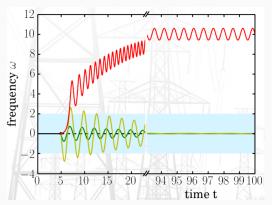
$$\frac{2H}{\omega}\frac{d^2\theta}{dt^2} = P_m - P_e$$

It is now clear what will happen if $P_m \neq P_e$.

Networks of synchronous machines

Networks of oscillators, i.e. an oscillator with angle θ_i at every node, can be studied. We get using a simplification of the load flow equations for P_e

$$\frac{2H_i}{\omega_i}\frac{d^2\theta_i}{dt^2} = P_m - \sum_j \frac{1}{x_{ij}}\sin(\theta_i - \theta_j)$$



The solutions have several interesting properties: basins of stability, limit cycles, etc. We can study them in a

simpler physics model called the Kuramoto model.

Source: Paul Schultz

This very similar model for synchronization was introduced in 1975 by Kuramoto:

$$rac{d heta_i}{dt} = \omega_i + rac{\kappa}{N}\sum_{j=1}^N \sin(heta_j - heta_i)$$

where θ_i is a phase, K is the coupling strength, multiplied by the sine of the phase differences, and ω_i is the natural frequency of the oscillator.

Suppose the natural frequencies are distributed with pdf $g(\omega)$.

To understand synchronisation in this model, Kuramoto introduced order parameters R and ψ defined by

$$Re^{i\psi(t)} = rac{1}{N}\sum_{j=1}^{N}e^{i heta_j(t)}$$

Kuramoto model

This allows us to re-write the equations as

$$\frac{d\theta_i}{dt} = \omega_i + \frac{KR}{N}\sin(\psi - \theta_i)$$

Now the interaction with the other θ_i is concealed inside the ψ .

The coupling between the θ_i grows with R; if R = 0 there is no synchrony and the phases are smeared around the circle. If $R \sim 1$ then the phases are synchronized.

We will show that the oscillators with $|\omega_i| \leq KR$ are locked at $\theta_i = \arcsin(\frac{\omega_i}{KR})$, whereas those with $|\omega_i| > KR$ are drifting.

See also: https://en.wikipedia.org/wiki/Kuramoto_model, http://www.stevenstrogatz.com/articles/

from-kuramoto-to-crawford-exploring-the-onset-of-synchronizatio
https://arxiv.org/abs/1511.07139,

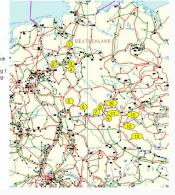
http://scala.uc3m.es/publications_MANS/PDF/finalKura.pdf

Videos: https://www.youtube.com/watch?v=sROKYelaWbo, https://www.youtube.com/watch?v=eAXVa__XWZ8,

Cycles Flows and Grid Outages

Line Outages

Zeit Leitung 1 22:10:13 380 Wehrendorf-Landesbergen 2 22:10:15 220 Bielefeld/Ost-Spexard 3 22:10:19 380 Bechterdissen-Elsen 4 22:10:22 220 Paderborn/Süd. Bechterdissen/Gütersloh 5 22:10:22 380 Dipperz-Großkrotzenburg 6 22:10:25 380 Großkrotzenburg Dipperz 2 7 22:10:27 380 Oberhaid-Grafenrheinfeld 8 22:10:27 380 Redwitz-Raitersaich 9 22:10:27 380 Redwitz-Oberhaid 10 22:10:27 380 Redwitz-Etzenricht 11 22:10:27 220 Würgau-Redwitz 12 22:10:27 380 Etzenricht-Schwandorf 13 22:10:27 220 Mechlenreuth Schwandorf 14 22:10:27 380 Schwandorf-Pleinting



When there are faults in the network, transmission lines can disconnect. This forces power flows onto the remaining network. If there is insufficient capacity, there can be a cascading line outage.

This happened in November 2006, where a cascading line outage caused the European network to split into three isolated parts, causing a major blackout.

Such outages may be exacerbated by high levels of variable renewable energy.

Recall that for net power injections p_n at nodes n, flows f_{ℓ} on lines ℓ , network incidence matrix K and cycle basis C (kernel of K, KC = 0) we can express Kirchoff's Circuit Laws as:

- Kirchoff's Current Law (KCL): $\mathbf{p} = K\mathbf{f}$
- Kirchoff's Voltage Law (KVL): $C^t X \mathbf{f} = 0$

Using voltage angle θ_n for each node and then using $f_l = \frac{\theta_i - \theta_j}{x_l}$:

$$\mathbf{f} = X^{-1} K^t \theta \qquad (\sim E = -\nabla \phi)$$

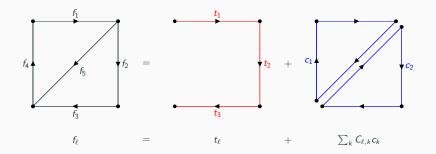
$$\mathbf{p} = K X^{-1} K^t \theta \qquad (\sim \rho = \Delta \phi)$$

NB: $KX^{-1}K^t$ is a weighted Laplacian matrix for the graph, so the final equation has the form of a discrete Poisson equation sourced by **p**.

Cycle formulation of linear power flow

We can use dual graph theory to decompose the flows in the network into two parts:

- 1. A flow on a spanning tree of the network, uniquely determined by nodal ${\bf p}$ (ensuring KCL)
- 2. Cycle flows, which don't affect KCL; their strength is fixed by enforcing KVL



The N-1 tree flows **t** are determined directly from the N nodal powers p_n and the network power balance constraint $\sum_n p_n = 0$.

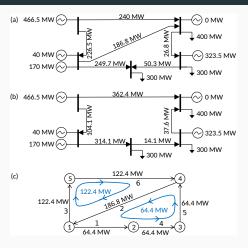
We solve for the L - N + 1 cycle flows c_k by enforcing the L - N + 1 KVL equations:

 $C^{t}X\mathbf{f} = C^{t}X(\mathbf{t} + C\mathbf{c}) = 0$

The matrix C is the incidence matrix of the weak dual graph, $C^{t}XC$ is the weighted Laplacian of the dual graph and the above equation becomes a discrete Poisson equation:

$$C^{t}XC\mathbf{c} = -C^{t}X\mathbf{t}$$

Line outages from cycles



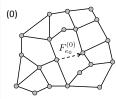
The outage of a line only affects the cycle flows.

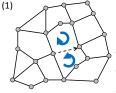
(a) shows the flows before the outage;

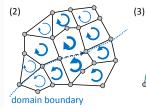
(b) shows the flows after the outage of the diagonal line;(c) shows the change in flows, decomposed into cycle flows.

Therefore the effect of the line outage on the other flows in the network can be entirely understood in terms of the cycle flows, corresponding to the nodes of the weak dual graph.

Line outages from cycles







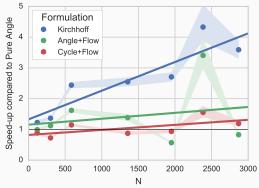
flow changes

If we consider the outage of a line, the change in flows can be expressed very compactly in terms of the change in the cycles flows, Δc , which are determined by a Poisson equation sourced by a term **q** that only has non-zero entries for cycles bordering the failed line

$$C^{t}XC\Delta \mathbf{c} = \mathbf{q}$$

For a plane network where the line fails away from the boundary, **q** is a dipole source for the two cycles that border the failed line.

Line outages from cycles



If we reformulate the linear optimal power flow using cycle flows instead of voltage angles we find:

- A speed-up of up to 20 times
- Average speed-up of factor 3
- Speed-up is highest for large networks with lots of decentralised generators

Oral examination sample questions

The following question are *not* identical to the oral exam, but give an indication of the difficulty level of the questions.

General Questions

- Describe variations of wind and solar in space and time (lecture 1)
- Describe what you would expect from the Fourier transform of wind and solar time series (lecture 1)
- What are the options for balancing variable renewables?
- What happens to feed-in when integrated over larger areas? (lecture 2)
- When balancing with only storage, how does storage volume depend on frequency of variations for a sinusoidal generation pattern? (lecture 4, sheet 2)
- When balancing only with networks, how does network distance depend on wavelength of variations?

- What is the incidence matrix? Write down the incidence matrix of a given network. (lecture 2)
- What is the Laplacian? (lecture 2)
- How do power, voltage angles and Laplacian relate for a linear power flow calculation? (lecture 3)
- How is the PTDF derived? (lecture 3)

Optimisation

- Write down the typical form of an optimisation problem. (lecture 6)
- What are the KKT conditions? (lecture 6)
- Describe each KKT condition. (lecture 6)
- Write down KKT for a given two-node problem. (lecture 8)
- Screening curves, demand duration curve: derive generation fleet for given parameters (lecture 8, sheet 4)
- Explain the merit order effect (lecture 10, 11)
- Show that for an investment optimisation for a single node with several generators that every generator makes back their costs (lecture 10)

- Write down the relation between storage dispatch/storing and energy. (lecture 4)
- How is Demand Side Management different from Storage? (lecture 5)
- Describe the opportunities of coupling to other energy sectors (lecture 9)
- Spatial scale (lecture 11)
- Describe the concept and application of flow tracing in power networks. (lecture 12)